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INTERNATIONAL PRELIMINARY EXAMINATION REPORT

(PCT Article 36 and Rule 70)

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Applicant's or agent's file reference PD-202131	FOR FURTHER ACTION See Notification of Transmittal of International Preliminary Examination Report (Form PCT/IPEA/416)	
International application No. PCT/US03/33130	International filing date (day/month/year) 17 October 2003 (17.10.2003)	Priority date (day/month/year) 25 October 2002 (25.10.2002)
International Patent Classification (IPC) or national classification and IPC IPC(7): H03F 3/58 and US Cl.: 330/43, 136, 149		
Applicant THE DIRECTTV GROUP, INC.		

1. This international preliminary examination report has been prepared by this International Preliminary Examining Authority and is transmitted to the applicant according to Article 36.
2. This REPORT consists of a total of 3 sheets, including this cover sheet.
☒ This report is also accompanied by ANNEXES, i.e., sheets of the description, claims and/or drawings which have been amended and are the basis for this report and/or sheets containing rectifications made before this Authority (see Rule 70.16 and Section 607 of the Administrative Instructions under the PCT).

These annexes consist of a total of 12 sheets.

3. This report contains indications relating to the following items:
 - I ☒ Basis of the report
 - II ☐ Priority
 - III ☐ Non-establishment of report with regard to novelty, inventive step and industrial applicability
 - IV ☐ Lack of unity of invention
 - V ☒ Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement
 - VI ☐ Certain documents cited
 - VII ☐ Certain defects in the international application
 - VIII ☐ Certain observations on the international application

Date of submission of the demand 24 May 2004 (24.05.2004)	Date of completion of this report 17 March 2005 (17.03.2005)
Name and mailing address of the IPEA/US Mail Stop PCT, Attn: IPEA/ US Commissioner for Patents P.O. Box 1450 Alexandria, Virginia 22313-1450 Facsimile No. (703) 305-3230	Authorized officer Steven J. Mottola <i>James R. Matthews</i> Telephone No. 703-308-0956

Form PCT/IPEA/409 (cover sheet)(July 1998)

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INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No.

PCT/US03/33130

I. Basis of the report

1. With regard to the elements of the international application:*

☐

the international application as originally filed.

☒

the description:

pages 2-30,33,34,36-38 as originally filedpages NONE, filed with the demandpages 1,31,32 and 35, filed with the letter of 10 November 2004 (10.11.2004)☒

the claims:

pages NONE, as originally filedpages NONE, as amended (together with any statement) under Article 19pages NONE, filed with the demandpages 39-46, filed with the letter of 10 November 2004 (10.11.2004)☒

the drawings:

pages 1-23, as originally filedpages NONE, filed with the demandpages NONE, filed with the letter of _____.☐

the sequence listing part of the description:

pages NONE, as originally filedpages NONE, filed with the demandpages NONE, filed with the letter of _____.

2. With regard to the language, all the elements marked above were available or furnished to this Authority in the language in which the international application was filed, unless otherwise indicated under this item.

These elements were available or furnished to this Authority in the following language _____ which is:

☐

the language of a translation furnished for the purposes of international search (under Rule 23.1(b)).

☐

the language of publication of the international application (under Rule 48.3(b)).

☐

the language of the translation furnished for the purposes of international preliminary examination (under Rules 55.2 and/or 55.3).

3. With regard to any nucleotide and/or amino acid sequence disclosed in the international application, the international preliminary examination was carried out on the basis of the sequence listing:

☐

contained in the international application in printed form.

☐

filed together with the international application in computer readable form.

☐

furnished subsequently to this Authority in written form.

☐

furnished subsequently to this Authority in computer readable form.

☐

The statement that the subsequently furnished written sequence listing does not go beyond the disclosure in the international application as filed has been furnished.

☐

The statement that the information recorded in computer readable form is identical to the written sequence listing has been furnished.

4. ☐ The amendments have resulted in the cancellation of:☐the description, pages NONE☐the claims, Nos. NONE☐the drawings, sheets/fig NONE5. ☐ This report has been established as if (some of) the amendments had not been made, since they have been considered to go beyond the disclosure as filed, as indicated in the Supplemental Box (Rule 70.2(c)).**

* Replacement sheets which have been furnished to the receiving Office in response to an invitation under Article 14 are referred to in this report as "originally filed" and are not annexed to this report since they do not contain amendments (Rules 70.16 and 70.17).

** Any replacement sheet containing such amendments must be referred to under item 1 and annexed to this report.

INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International Application No.
PCT/US03/331

V. Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

1. STATEMENT

Novelty (N)	Claims <u>1-48</u>	YES
	Claims <u>NONE</u>	NO
Inventive Step (IS)	Claims <u>1-48</u>	YES
	Claims <u>NONE</u>	NO
Industrial Applicability (IA)	Claims <u>1-48</u>	YES
	Claims <u>NONE</u>	NO

2. CITATIONS AND EXPLANATIONS

Claims 1-48 meet the criteria set out in PCT Article 33(2)-(3), because the prior art does not teach or fairly suggest measuring the nonlinearity of a TWTA and computing an RMS value of an input signal used to measure the nonlinearity of the TWTA to obtain an input and an output operating point of the TWTA.

Claims 1-48 meet the criteria set out in PCT Article 33(4), and thus have industrial applicability because the subject matter claimed can be made or used in industry.

ESTIMATING THE OPERATING POINT ON A NONLINEAR TRAVELING
WAVE TUBE AMPLIFIER

CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] This application claims the benefit under 35 U.S.C. §119(e) of the following U.S. Provisional Patent Applications, which are incorporated by reference herein:

[0002] U.S. Provisional Patent Application No. 60/421,289, filed October 25, 2002
5 by Ernest C. Chen and Shamik Maitra, entitled "ESTIMATING THE OPERATING
POINT ON A NONLINEAR TRAVELING WAVE TUBE AMPLIFIER", attorney's
docket number PD-202131; and

[0003] U.S. Provisional Patent Application No. 60/510,368, filed on October 10,
2003, by Ernest C. Chen, entitled "IMPROVING TWTA AM-AM AND AM-PM
10 MEASUREMENT", attorney's docket number PD-202118.

[0004] This is a continuation-in-part application and claims the benefit under 35
U.S.C. §120 of the following co-pending and commonly-assigned U.S. utility patent
applications, which are incorporated by reference herein:

[0005] Utility Application Serial No. 09/844,401, filed April 27, 2001, by Ernest C.
15 Chen, entitled "LAYERED MODULATION FOR DIGITAL SIGNALS," attorneys'
docket number PD-200181; and

[0006] U.S. Application Serial No. 10/165,710, filed on June 7, 2002, by Ernest C.
Chen, entitled "SATELLITE TWTA ON-LINE NON-LINEARITY
MEASUREMENT," attorney's docket number PD-200228.

BACKGROUND OF THE INVENTION

1. Field of the Invention

[0007] The present invention relates to systems and methods for transmitting data,
and in particular to a system and method for estimating a traveling wave tube
25 amplifier operating point to accurately reproduce transmitted signals.

refers to the reconstructed clean signal before the imposition of TWTA nonlinearity. The RMS value identifies the input operating point on the measured nonlinearity curves.

5 [0008] The output operating point is then obtained at step 1306 (e.g., as a byproduct of the non-linearity measurement data). The output operating point may be obtained using a variety of methods. For example, the output operating point may be calculated from the RMS value of the output (received) values used to determine the TWTA non-linearity curve (e.g., when matching the curve as described below) less the estimated noise power value. The output operating point may also be obtained from 10 the corresponding point on the measured TWTA non-linearity curves. With the input and output operating points obtained, the upper layer signal (of a layered modulation) may be more accurately reconstructed as part of the layered modulation scheme.

[0009] It should be noted that the measurement of non-linearity (i.e., step 1302) may be conducted in a variety of manners as part of the layered modulation scheme. 15 Nonetheless, regardless of the technique used to measure non-linearity, the operating point is estimated along with the measurement for the non-linearity curves. The TWTA non-linearity may be measured at the local IRDs 500, in which case the operating point may be automatically calculated from the nonlinearity measurements. The TWTA non-linearity may also be made at a broadcast/uplink center 104 with the 20 operating point similarly obtained, in which case information on TWTA non-linearity and operating point can be downloaded to individual IRDs 500, such as through the downlink signal 118, to support the layered modulation signal receiving process.

6. Measuring Non-Linearity

25 [0010] As described above, the measurement of non-linearity (i.e., step 1302) may be conducted in a variety of manners as part of the layered modulation scheme. A first mechanism for TWTA non-linearity measurement is fully described in United States Patent Application Serial No. 10/165,710, entitled "SATELLITE TWTA ON-

LINE NON-LINEARITY MEASUREMENT", filed on June 7, 2002 by Ernest C.

Chen. A second measurement mechanism is fully described in United States

Provisional Patent Application Serial No. 60/510,368, entitled "IMPROVING TWTA
AM-AM AND AM-PM MEASUREMENT", filed on October 10, 2003, by Ernest C.

5 Chen. The second mechanism represents an improvement over the first mechanism.
Non-linearity may be measured in each local IRD 500 (e.g., using a coherent
averaging technique that maximizes signal processing gains).

[0011] TWTA non-linearity may be measured locally within individual IRDs. This
may, eliminate the need to transmit the non-linearity curves from the broadcast/uplink
10 center 104. TWTA non-linearity can also be measured at the broadcast/uplink center
104 using a similar estimation procedure as that described above but possibly with a
larger receive antenna for increased CNR as desired. The IRD 802 which receives the
downlink signal 118 (e.g., from the LNB 502) may also include a signal processor
which extracts the symbol stream and carrier frequency from the incoming signal and
15 generates an ideal signal, i.e. a signal without the effects of the TWTA and noise. The
ideal signal is then used in a comparison processor to produce TWTA characteristic
maps (which provide the measurements for TWTA non-linearity). As described
herein, the signal processor and comparison processor may be incorporated in IRD
802 within the tuner/demodulator 904, FEC 506. The details concerning the
20 generation of the characteristic maps will be described below in the discussion of
FIGs. 14A - 14C.

[0012] Typically, the TWTA characteristic maps comprise measurements of the
output amplitude modulation versus the input amplitude modulation (the AM-AM
map) and the output phase modulation versus the input amplitude modulation (the
25 AM-PM map). The received signal represents the TWTA amplifier output (plus
noise) and the generated ideal signal represents the amplifier input. In addition to
diagnosing and monitoring the amplifier, these characteristic maps may then be used

reconstruction of the upper layer signal during the signal reconstruction and cancellation process. Such an offset does not alter the performance of layered modulation processing (or non-linearity compensation performance). In fact, offsetting the operating point may result in a simple and consistent representation of TWTA non-linearity regardless of input saturation, input backoff, etc.

[0013] To offset the measurement curves, the input and output amplitude values (i.e., used during the non-linearity curve measurement) may be rescaled so that the operating point is at a desired reference point (e.g., 0 dB), for both input and output (e.g., thereby providing referenced operating point values). In the log domain, such rescaling may be performed by subtracting the measured (AM) input operating point value (in dB) from all input values (in dB). Likewise, the measured output (AM) operating point value (in dB) may be subtracted from values of all output points (in dB). Thus, by offsetting the measurement curves, the curves may be more easily referenced. In silicon and other hardware implementations, however, it may be desirable to scale the input and output operating points or signals back (e.g., to -3 dB or -5 dB) to avoid signal saturation or fractional value representation overflow for incoming and outgoing signals. The shifting process can be done similarly to that described above.

[0014] With a shifted AM scale as desired, the output PM value may also be rescaled by subtracting the measured (angular) phase value at the output operating point from the phase value of all output points.

[0015] The results of the above scaling is that the operating point will provide reference values, such as (0 dB, 0 dB) for the AM-AM map, and (0dB, 0°) for the AM-PM map. In this case the input signal must be scaled to 0 dB to match the operating point. To guard against signal saturation errors (and to avoid the need for a look-up-table [LUT] extrapolation), bounding points may be placed beyond the measured signal interval to allow interpolation of the input data (or output testing data) in the testing process that falls outside of the range of a TWTA measurement

WHAT IS CLAIMED IS:

1. A method for determining an input operating point and an output operating point on a non-linear traveling wave tube amplifier (TWTA), comprising:
measuring non-linearity of the TWTA;
5 computing an input root-mean-square (RMS) value of an input signal used to measure the non-linearity of the TWTA, wherein the input RMS value identifies an input operating point of the measured non-linearity of the TWTA; and
obtaining an output operating point.
- 10 2. The method of claim 1, wherein the measuring the non-linearity of the TWTA comprises measuring the non-linearity at a local receiver.
3. The method of claim 1, wherein the measuring the non-linearity of the TWTA comprises measuring the non-linearity at a broadcast center.
15
4. The method of claim 3, further comprising downloading the measured non-linearity and the output operating point to an individual receiver.
- 20 5. The method of claim 1, wherein obtaining the output operating point comprises calculating an output RMS value of output signals used in measuring the non-linearity of the TWTA.
- 25 6. The method of claim 1, wherein obtaining the output operating point comprises obtaining a corresponding point on the measured TWTA non-linearity based on the input RMS value.
7. The method of claim 1, further comprising reconstructing an upper layer signal of a layered modulation based on the output operating point.

8. The method of claim 1, further comprising offsetting the measured non-linearity to provide referenced operating point values.

5 9. The method of claim 8, wherein the offsetting comprises scaling an input amplitude value and output amplitude value of the measured non-linearity of the TWTA to place the input and output operating points at desired points.

10 10. The method of claim 9, wherein the scaling comprises subtracting a measured input operating point value from all input values in a log domain.

11. The method of claim 9, wherein the scaling comprises subtracting a measured output operating point value from all output values in a log domain.

15 12. The method of claim 9, wherein the scaling comprises subtracting a measured phase value at the output operating point from phase values of all output points used to measure the non-linearity of the TWTA.

20 13. The method of claim 9, wherein the scaling further comprises:
placing bounding points beyond end points used to measure the non-linearity;
and
interpolating output testing data that falls outside of the measured non-linearity based on the bounding points.

25 14. The method of claim 8, further comprising mapping the input operating point and output operating point to a particular level to avoid signal saturation or fractional value representation overflow.

15. An apparatus for determining an input operating point and an output operating point on a non-linear traveling wave tube amplifier (TWTA), comprising:

means for measuring a non-linearity of the TWTA;

5 means for computing an input root-mean-square (RMS) value of an input signal used to measure the non-linearity of the TWTA, wherein the input RMS value identifies an input operating point of the measured non-linearity of the TWTA; and

means for obtaining an output operating point.

10 16. The apparatus of claim 15, wherein the means for measuring the non-linearity of the TWTA comprises means for measuring the non-linearity at a local receiver.

15 17. The apparatus of claim 15, wherein the means for measuring the non-linearity of the TWTA comprises means for measuring the non-linearity at a broadcast center.

18. The apparatus of claim 17, further comprising means for downloading the measured non-linearity and the output operating point to an individual receiver.

20 19. The apparatus of claim 15, wherein the means for obtaining the output operating point comprises means for calculating an output RMS value of output signals used in measuring the non-linearity of the TWTA.

25 20. The apparatus of claim 15, wherein the means for obtaining the output operating point comprises means for obtaining a corresponding point on the measured TWTA non-linearity based on the input RMS value.

21. The apparatus of claim 15, further comprising means for reconstructing an upper layer signal of a layered modulation based on the output operating point.

5 22. The apparatus of claim 15, further comprising means for offsetting the measured non-linearity to provide referenced operating point values.

23. The apparatus of claim 22, wherein the means for offsetting comprises means for scaling an input amplitude value and output amplitude value of the measured non-linearity of the TWTA to place the input and output operating point at
10 desired points.

24. The apparatus of claim 23, wherein the means for scaling comprises means for subtracting a measured input operating point value from all input values in a log domain.
15

25. The apparatus of claim 23, wherein the means for scaling comprises means for subtracting a measured output operating point value from all output values in a log domain.

20 26. The apparatus of claim 23, wherein the means for scaling comprises means for subtracting a measured phase value at the output operating point from phase values of all output points used to measure the non-linearity of the TWTA.

25 27. The apparatus of claim 23, wherein the means for scaling further comprises:
means for placing bounding points beyond end points used to measure the non-linearity; and

means for interpolating output testing data that falls outside of the measured non-linearity based on the bounding points.

28. The apparatus of claim 22, further comprising means for mapping the input operating point and output operating point to a particular level to avoid signal saturation or fractional value representation overflow.

29. A system for determining an input operating point and an output operating point on a non-linear traveling wave tube amplifier (TWTA), comprising:

10 (a) a measuring module configured to:

(1) measure non-linearity of the TWTA; and

(2) obtaining an output operating point; and

(b) a non-linear distortion map module configured to compute an input root-mean-square (RMS) value of an input signal used to measure the non-linearity of the TWTA, wherein the RMS value identifies an input operating point of the measured non-linearity of the TWTA.

30. The system of claim 29, wherein the measuring module is located at a local receiver.

31. The system of claim 29, wherein the measuring module is located at a broadcast center.

32. The system of claim 31, further comprising a receiver configured to download the measured non-linearity and the output operating point.

33. The system of claim 29, wherein the measuring module is configured to obtain the output operating point by calculating an output RMS value of output signals used in measuring the non-linearity of the TWTA.

5 34. The system of claim 29, wherein the measuring module is configured to obtain the output operating point by obtaining a corresponding point on the measured TWTA non-linearity based on the input RMS value.

10 35. The system of claim 29, further comprising a receiver configured to reconstruct an upper layer signal of a layered modulation based on the output operating point.

15 36. The system of claim 29, further comprising a receiver configured to offset the measured non-linearity to provide referenced operating point values.

20 37. The system of claim 36, wherein the receiver is configured to offset the measured non-linearity by scaling an input amplitude value and output amplitude value of the measured non-linearity of the TWTA to place the input and output operating point at desired points.

38. The system of claim 37, wherein the receiver is configured to scale by subtracting a measured input operating point value from all input values in a log domain.

25 39. The system of claim 37, wherein the receiver is configured to scale by subtracting a measured output operating point value from all output values in a log domain.

40. The system of claim 37, wherein the receiver is configured to scale by subtracting a measured phase value at the output operating point from phase values of all output points used to measure the non-linearity of the TWTA.

5 41. The system of claim 37, wherein the receiver is further configured to scale by:
placing bounding points beyond end points used to measure the non-linearity;
and
interpolating output testing data that falls outside of the measured non-linearity
10 based on the bounding points.

42. The system of claim 36, wherein the receiver is further configured to map the input operating point and output operating point to a particular level to avoid signal saturation or fractional value representation overflow.

15 43. The method of claim 2, wherein the step of measuring the non-linearity of the TWTA comprises:
generating a difference between an ideal signal and a received signal.

20 44. The method of claim 43, wherein generating a difference between an ideal signal and a received signal comprises:
demodulating the received signal;
decoding the demodulated signal;
generate the ideal signal; and
25 subtracting the ideal signal from the demodulated signal.

45. The method of claim 43, wherein generating a difference between an ideal signal and a received signal comprises:

- demodulating the received signal;
- decoding the demodulated signal;
- 5 generating the ideal signal with a carrier of the received signal;
- subtracting the ideal signal from the received signal.

46. The method of claim 2, wherein the means for of measuring the non-linearity of the TWTA comprises:

- 10 generating a difference between an ideal signal and a received signal.

47. The method of claim 43, wherein generating a difference between an ideal signal and a received signal comprises:

- demodulating the received signal;
- 15 decoding the demodulated signal;
- generate the ideal signal; and
- subtracting the ideal signal from the demodulated signal.

48. The method of claim 43, wherein generating a difference between an ideal signal and a received signal comprises:

- 20 demodulating the received signal;
- decoding the demodulated signal;
- generating the ideal signal with a carrier of the received signal;
- subtracting the ideal signal from the received signal.

25

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